

The effects of variable fluid properties on thin film stability

Serge D'Alessio¹, Cam Seth¹, J.P. Pascal²

¹University of Waterloo, Faculty of Mathematics, Waterloo, Canada

²Ryerson University, Department of Mathematics, Toronto, Canada

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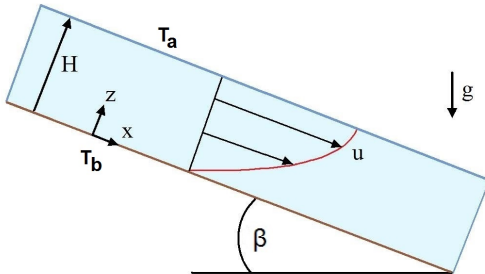
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Problem description

The stability of two-dimensional laminar flow of a thin fluid layer down a heated inclined surface has been investigated



Previous work

- ▶ Isothermal case: Benjamin (1957), Yih (1963) and Benney (1966)
- ▶ Non-isothermal case: variable surface tension - Trevelyan *et al.* (2007) & D'Alessio *et al.* (2010)
variable viscosity - Goussis & Kelly (1985) and Hwang & Weng (1988)
variable surface tension & viscosity - Kabova & Kuznetsov (2002)
- ▶ Pascal *et al.* (2013) considered variable density, viscosity, surface tension, thermal conductivity and specific heat for small parameter variations

Governing equations

In the absence of viscous dissipation, the governing equations for a fluid possessing variable fluid properties are given by:

$$\rho \frac{D\rho}{Dt} + \rho \left(\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) = 0$$

$$\rho \frac{Du}{Dt} = -\frac{\partial p}{\partial x} + g\rho \sin \beta + \frac{\partial}{\partial x} \left[2\mu \frac{\partial u}{\partial x} - \frac{2}{3}\mu \left(\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) \right] + \frac{\partial}{\partial z} \left[\mu \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \right]$$

$$\rho \frac{Dw}{Dt} = -\frac{\partial p}{\partial z} - g\rho \cos \beta + \frac{\partial}{\partial z} \left[2\mu \frac{\partial w}{\partial z} - \frac{2}{3}\mu \left(\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) \right] + \frac{\partial}{\partial x} \left[\mu \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \right]$$

$$\rho \frac{D(c_p T)}{Dt} = \frac{\partial}{\partial x} \left(K \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial z} \left(K \frac{\partial T}{\partial z} \right) - p \left(\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right)$$

Governing equations

Allow the fluid properties to vary linearly with temperature as follows (in dimensionless form):

$$\begin{aligned} \frac{\rho}{\rho_0} &= 1 - \alpha T && \text{density} \\ \frac{\mu}{\mu_0} &= 1 - \lambda T && \text{viscosity} \\ \frac{c_p}{c_{p0}} &= 1 + S T && \text{specific heat} \\ \frac{K}{K_0} &= 1 + \Lambda T && \text{thermal conductivity} \\ \frac{\sigma}{\sigma_0} &= 1 - \gamma T && \text{surface tension} \end{aligned}$$

Here, α , γ , λ , Λ , S are positive dimensionless parameters measuring the rate of change with respect to temperature and ρ_0 , μ_0 , c_{p0} , K_0 , σ_0 represent values at the reference temperature T_a (or $T = 0$ in dimensionless form).

Dimensionless equations

To cast the equations in dimensionless form the following scales are used. The length scale is the Nusselt thickness given by:

$$H = \left(\frac{3\mu_0 Q}{g\rho_0 \sin \beta} \right)^{1/3}$$

corresponding to a uniform steady isothermal flow.

Here, Q is the constant volume flux.

The pressure scale is $\rho_0 U^2$ with $U = Q/H$.

The time scale is H/U .

The temperature scale is $\Delta T = T_b - T_a$.

Dimensionless equations

Using the Boussinesq approximation and in dimensionless form the equations become:

$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

$$Re \frac{Du}{Dt} = -Re \frac{\partial p}{\partial x} + 3(1 - \alpha T) + \frac{\partial}{\partial x} \left((1 - \lambda T) \frac{\partial u}{\partial x} \right) + \frac{\partial}{\partial z} \left((1 - \lambda T) \frac{\partial u}{\partial z} \right) - \lambda \frac{\partial T}{\partial x} \frac{\partial u}{\partial x} - \lambda \frac{\partial T}{\partial z} \frac{\partial w}{\partial x}$$

$$Re \frac{Dw}{Dt} = -Re \frac{\partial p}{\partial z} - 3 \cot \beta (1 - \alpha T) + \frac{\partial}{\partial x} \left((1 - \lambda T) \frac{\partial w}{\partial x} \right) + \frac{\partial}{\partial z} \left((1 - \lambda T) \frac{\partial w}{\partial z} \right) - \lambda \frac{\partial T}{\partial x} \frac{\partial u}{\partial z} - \lambda \frac{\partial T}{\partial z} \frac{\partial w}{\partial z}$$

$$PrRe \frac{DT}{Dt} [(1 + S/\Delta T_r)T + ST^2] = \frac{\partial}{\partial x} [(1 + \Lambda T) \frac{\partial T}{\partial x}] + \frac{\partial}{\partial z} [(1 + \Lambda T) \frac{\partial T}{\partial z}]$$



Boundary conditions

The dynamic conditions along the free surface, $z = h(x, t)$, are:

$$p = \frac{2(1-\lambda T)}{ReF} \left(\left[\frac{\partial h}{\partial x} \right]^2 \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} - \frac{\partial h}{\partial x} \frac{\partial u}{\partial z} - \frac{\partial h}{\partial x} \frac{\partial w}{\partial x} \right) - \frac{(We - MaT)}{F^{3/2}} \frac{\partial^2 h}{\partial x^2}$$

$$-MaRe\sqrt{F} \left(\frac{\partial T}{\partial x} + \frac{\partial h}{\partial x} \frac{\partial T}{\partial z} \right) = (1 - \lambda T) \left[G \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) - 4 \frac{\partial h}{\partial x} \frac{\partial u}{\partial x} \right]$$

$$\text{where } F = 1 + \left[\frac{\partial h}{\partial x} \right]^2, \quad G = 1 - \left[\frac{\partial h}{\partial x} \right]^2$$

Based on Newton's Law of Cooling, the heat transfer across the free surface can be expressed as:

$$-Bi\sqrt{F}T = (1 + \lambda T) \left(\frac{\partial T}{\partial z} - \frac{\partial h}{\partial x} \frac{\partial T}{\partial x} \right)$$

Boundary conditions

The kinematic condition along the free surface is given by:

$$w = \frac{\partial h}{\partial t} + u \frac{\partial h}{\partial x}$$

Lastly, the bottom temperature, no-slip and impermeability conditions are:

$$T = 1 \text{ at } z = 0$$

$$u = w = 0 \text{ at } z = 0$$

Dimensionless parameters

$$Re = \frac{\rho_0 UH}{\mu_0}$$

Reynolds number

$$We = \frac{\rho_0 U^2 H}{\sigma_0}$$

Weber number

$$Ma = \frac{\rho_0 U^2 H}{\gamma \Delta T}$$

Marangoni number

$$Pr = \frac{\rho_0 U^2 H}{\mu_0 c_{p0}}$$

Prandtl number

$$Bi = \frac{K_0}{\alpha_g H}$$

Biot number

$$\Delta T_r = \frac{T_b - T_a}{T_a}$$

Relative Temperature Difference

Also, α , λ , Λ , S represent dimensionless rates of change of density, viscosity, thermal conductivity and specific heat with respect to temperature.

Steady-state equations

Steady uniform flow in the streamwise direction is given by $h \equiv 1$, $w \equiv 0$, $u = u_s(z)$, $p = p_s(z)$, $T = T_s(z)$ and satisfies the following boundary-value problems ($D \equiv d/dz$):

$$D[(1+\Lambda T_s)DT_s] = 0, \quad (1+\Lambda T_s)DT_s + BiT_s = 0 \quad \text{at } z = 1, \quad T_s(0) = 1$$

$$D[(1-\lambda T_s)Du_s] + 3(1-\alpha T_s) = 0, \quad Du_s = 0 \quad \text{at } z = 1, \quad u_s(0) = 0$$

$$ReDp_s = -3 \cot\beta(1-\alpha T_s), \quad p_s(1) = 0$$

Steady-state solutions

The steady-state solutions are given by:

$$T_s(z) = \sqrt{a - bz} - \frac{1}{\Lambda}$$

$$u_s(z) = a_0 \ln \left(\frac{A - \lambda \sqrt{a - bz}}{A - \lambda \sqrt{a}} \right) + a_1 z - \frac{\alpha}{\lambda} z^2 + a_2 (\sqrt{a - bz} - \sqrt{a}) \\ + a_3 [(a - bz)^{3/2} - a^{3/2}]$$

$$p_s(z) = \frac{3 \cot \beta}{Re} \left(1 + \frac{\alpha}{\Lambda} \right) (1 - z) + \frac{2\alpha \cot \beta}{bRe} [(a - b)^{3/2} - (a - bz)^{3/2}]$$

where the constants a, b, a_0, a_1, a_2, a_3 and A are related to the parameters Λ, Bi, λ and α .

Steady-state solutions

Some special cases:

$$\Lambda = 0, \quad T_s(z) = 1 - \frac{Bi}{1 + Bi} z$$

For $Bi = 0$, $T_s(z) = 1$ while as $Bi \rightarrow \infty$, $T_s(z) \rightarrow 1 - z$

$$\text{For } Bi = 0, \quad u_s(z) = 3 \left(\frac{1 - \alpha}{1 - \lambda} \right) z \left(1 - \frac{z}{2} \right)$$

Perturbation equations

Next impose small disturbances on the steady-state flow:

$$u = u_s(z) + \tilde{u}(x, z, t), \quad w = \tilde{w}(x, z, t), \quad p = p_s(z) + \tilde{p}(x, z, t)$$

$$T = T_s(z) + \tilde{T}(x, z, t), \quad h = 1 + \eta(x, t)$$

Substitute these into the governing equations, linearize and assume the disturbances have the form:

$$(\tilde{u}, \tilde{w}, \tilde{p}, \tilde{T}, \eta) = (\hat{u}(z), \hat{w}(z), \hat{p}(z), \hat{T}(z), \hat{\eta})e^{ik(x-ct)}$$

where k (real & positive) represents the wavenumber of the perturbation and c is a complex quantity with the real part denoting the phase speed of the perturbation while the imaginary part is related to the growth rate.



Perturbation equations

The linearized perturbation equations become:

$$D\hat{w} + ik\hat{u} = 0$$

$$\begin{aligned} \operatorname{Re}[ik(u_s - c)\hat{u} + \hat{w}Du_s] &= -ik\operatorname{Re}\hat{p} + k^2(\lambda T_s - 1)\hat{u} \\ + D[(1 - \lambda T_s)D\hat{u}] - \lambda\hat{T}D^2u_s - \lambda Du_s D\hat{T} - ik\lambda\hat{w}DT_s - 3\alpha\hat{T} \\ ik\operatorname{Re}(u_s - c)\hat{w} &= -\operatorname{Re}D\hat{p} + 3\alpha \cot\beta \hat{T} - k^2(1 - \lambda T_s)\hat{w} \\ + D[(1 - \lambda T_s)D\hat{w}] - ik\lambda\hat{T}Du_s - \lambda DT_s D\hat{w} \\ \operatorname{Pr}\operatorname{Re}(1 + S/\Delta T_r + 2ST_s)[ik(u_s - c)\hat{T} + \hat{w}DT_s] \\ &= -k^2(1 + \lambda T_s)\hat{T} + D^2[(1 + \lambda T_s)\hat{T}] \end{aligned}$$

Boundary conditions

Along the free surface ($z = 1$) the perturbations satisfy:

$$\hat{p} = -\hat{\eta}Dp_s + \frac{2}{Re}(1 - \lambda T_s)D\hat{w} + k^2(We - MaT_s)\hat{\eta}$$

$$(1 - \lambda T_s)(\hat{\eta}D^2u_s + D\hat{u} + ik\hat{w}) = -ikMaRe(\hat{T} + \hat{\eta}DT_s)$$

$$D[(1 + \Lambda T_s)\hat{T}] + \hat{\eta}D[(1 + \Lambda T_s)DT_s + BiT_s] + Bi\hat{T} = 0$$

$$\hat{w} = ik(u_s - c)\hat{\eta}$$

while along the bottom the conditions are:

$$\hat{u}(0) = \hat{w}(0) = \hat{T}(0) = 0$$

Small wavenumber expansion

Recall that for isothermal flow small wavenumber perturbations are the most unstable. Assume this is also true for non-isothermal flow and expand the perturbations in the following series:

$$\hat{u} = u_0(z) + ku_1(z) + O(k^2)$$

$$\hat{w} = w_0(z) + kw_1(z) + O(k^2)$$

$$\hat{p} = p_0(z) + kp_1(z) + O(k^2)$$

$$\hat{T} = T_0(z) + kT_1(z) + O(k^2)$$

$$\hat{\eta} = \eta_0 + k\eta_1 + O(k^2)$$

$$c = c_0 + kc_1 + O(k^2)$$

This leads to a hierarchy of problems at various orders of k .

Neutral stability

With the help of the Maple Computer Algebra System an exact, but lengthy, expression for the critical Reynolds number, Re_{crit} , has been found having the functional form

$$Re_{crit}^* = f(\alpha, \lambda, \Lambda, \Delta T_r, S, Pr, Ma, Bi) \text{ where } Re_{crit}^* = \frac{Re_{crit}}{\cot\beta}$$

which predicts the onset of instability. With no heating the isothermal result, $Re_{crit}^* = 5/6$, is recovered. Re_{crit}^* does not depend on We (as is the case with isothermal flow).

Special case

For $Bi = 0$ the critical Reynolds number is given by

$$Re_{crit}^* = \frac{5(1-\lambda)^2}{6(1-\alpha)}$$

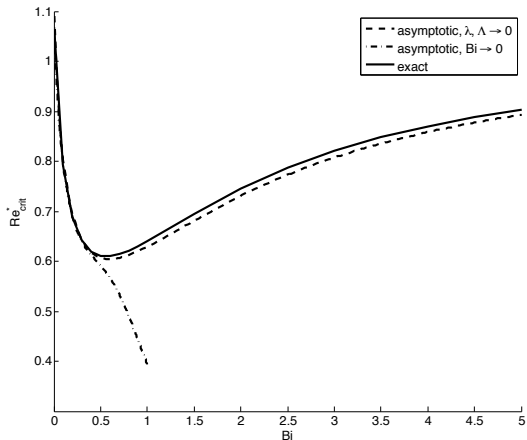
The dependence of Re_{crit}^* on α, λ can be explained by examining how the flow rate, Q , is influenced. Recall that

$$Q = \frac{\rho g \sin\beta H^3}{3\mu}$$

for steady uniform isothermal flow.

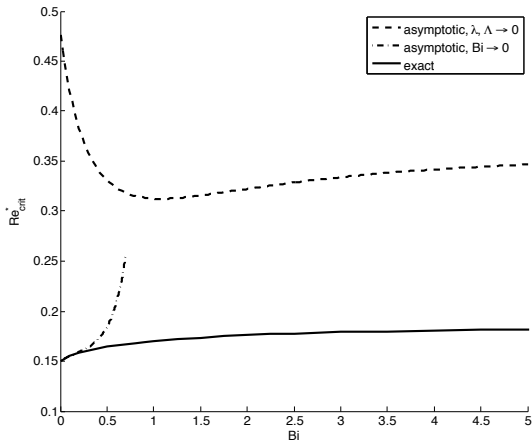
Comparisons with previous research

Comparison between our exact results and the asymptotic expansions of Pascal *et al.* (2013).
 Parameter values:
 $\alpha = 0.5$, $\lambda = 0.2$,
 $\Lambda = 0.25$, $S = 1$,
 $Ma = \Delta T_r = 1$,
 $Pr = 7$



Comparisons with previous research

Comparison between our exact results and the asymptotic expansions of Pascal *et al.* (2013).
 Parameter values:
 $\alpha = 0.5, \lambda = 0.7,$
 $\Lambda = 0.7, S = 1,$
 $Ma = \Delta T_r = 1,$
 $Pr = 7$



Comparisons with previous research

With $\lambda = \Lambda = \alpha = S = 0$ the expression for Re_{crit}^* becomes:

$$Re_{crit}^* = \frac{10(1 + Bi)^2}{5Ma Bi + 12(1 + Bi)^2}$$

which coincides with the result obtained by D'Alessio *et al.* (2010). Thus, thermocapillarity is destabilizing as Re_{crit}^* decreases with Ma . The scaled critical Reynolds number attains a minimum at $Bi = 1$, given by $Re_{crit,min}^* = 40/(48 + 5Ma)$. The limit as Bi tends to infinity is equal to the value at $Bi = 0$ which is given by $Re_{crit}^* = 5/6$ and corresponds to the isothermal case.

Variation in density

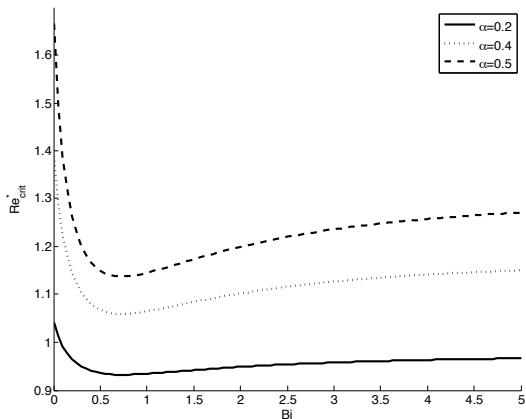
For $0 < Bi < \infty$ a negative temperature gradient within the fluid layer ensues which establishes a gravitationally unstable top-heavy density gradient within the fluid layer. Increasing α triggers competing stability mechanisms which is reflected in the Rayleigh number, Ra :

$$Ra = \frac{\hat{\alpha} g \cos\beta H^3 \Delta T}{\left(\frac{\mu}{\rho}\right) \left(\frac{K}{\rho c_p}\right)} = 3\rho_0 \cot\beta \left(\frac{\alpha \rho c_p Q}{K}\right)$$

Increasing α does not necessarily increase Ra since both ρ and Q decrease while holding c_p, K constant.

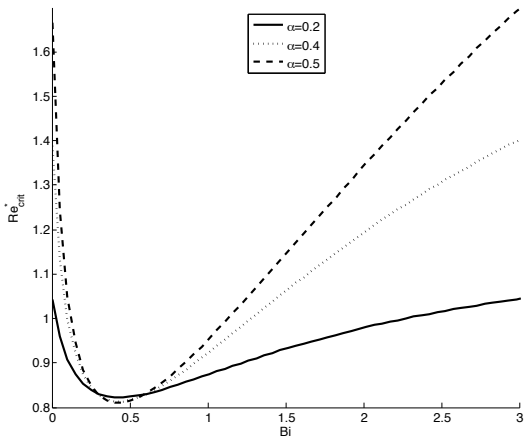
Variation in density

Parameter values:
 $\lambda = \Lambda = S = Ma = 0,$
 $\Delta T_r = 1, Pr = 7$



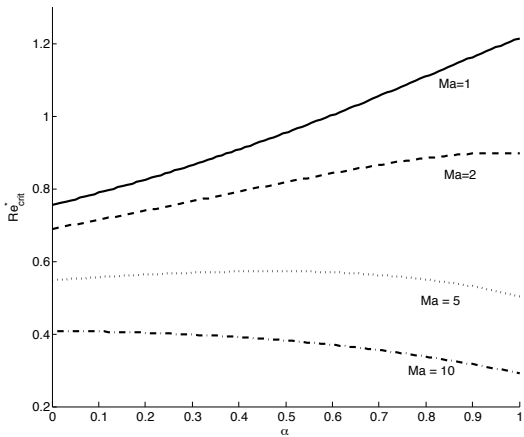
Variation in density

Parameter values:
 $\lambda = \Lambda = S = Ma = 0,$
 $\Delta T_r = 1, Pr = 30$



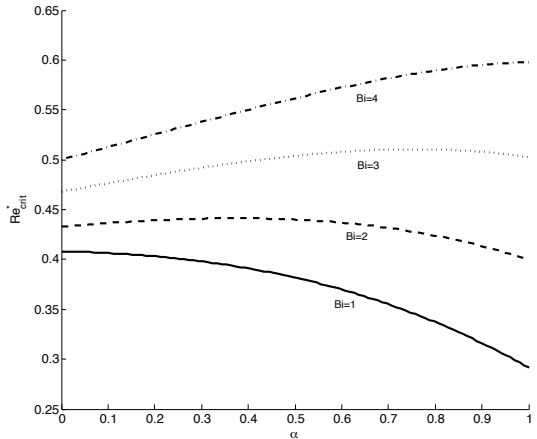
Marangoni effect

Parameter values:
 $\lambda = \Lambda = S = 0,$
 $Bi = 1, \Delta T_r = 1,$
 $Pr = 7$



Marangoni effect

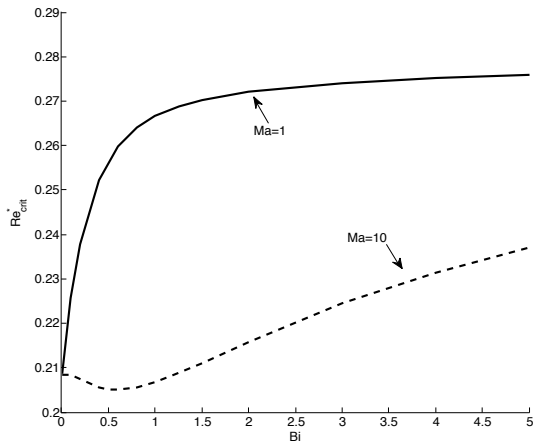
Parameter values:
 $\lambda = \Lambda = S = 0,$
 $Ma = 10, \Delta T_r = 1,$
 $Pr = 7$



Variation in viscosity

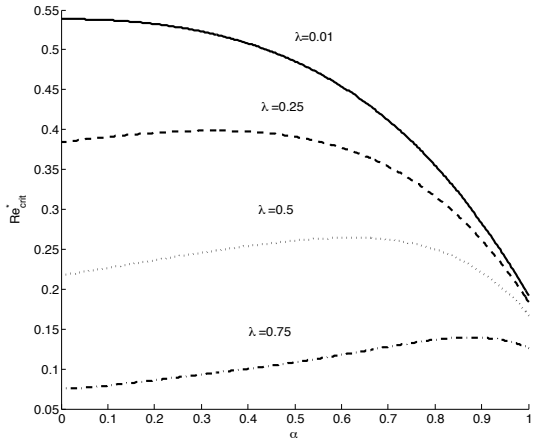
Parameter values:

$$\alpha = \Lambda = S = 0,$$
$$\lambda = 0.5, \Delta T_r = 1,$$
$$Pr = 7$$



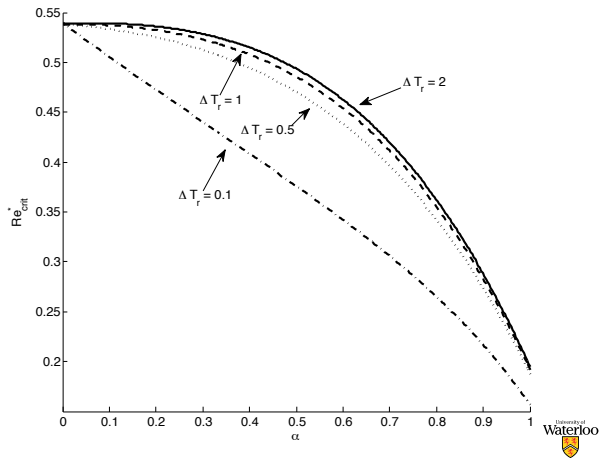
Variation in viscosity

Parameter values:
 $\Lambda = 0.5, S = 1,$
 $Bi = 0.25, Ma = 10,$
 $\Delta T_r = 1, Pr = 7$



Variation in ΔT_r

Parameter values:
 $\lambda = 0, \Lambda = 0.5, S = 1,$
 $Ma = 10, Bi = 0.25,$
 $Pr = 7$



Variation in S

Parameter values:

$$\Lambda = 0, Ma = 1,$$

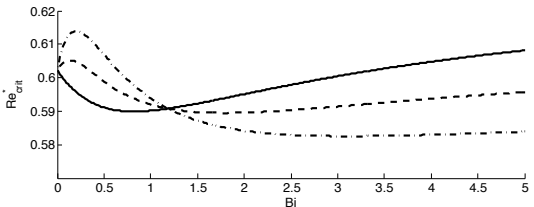
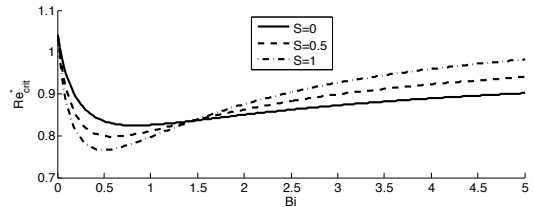
$$\Delta T_r = 1, Pr = 7$$

Top panel:

$$\alpha = 0.2, \lambda = 0$$

Bottom panel:

$$\alpha = 0, \lambda = 0.15$$



Variation in Λ

Parameter values:

$S = 0, Ma = 1,$

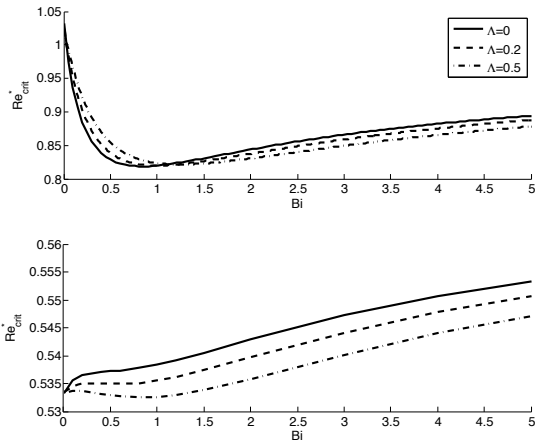
$\Delta T_r = 1, Pr = 7$

Top panel:

$\alpha = 0.2, \lambda = 0$

Bottom panel:

$\alpha = 0, \lambda = 0.2$

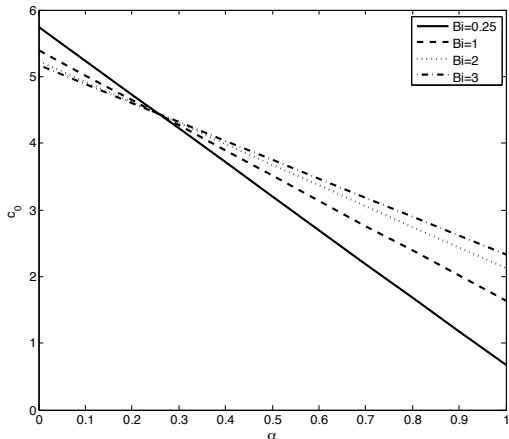


Variation in perturbation phase speed, c_0

Parameter values:

$$\lambda = \Lambda = 0.5$$

c_0 does not depend on $Ma, S, \Delta T_r, Pr$ and varies linearly with α



Variation in perturbation phase speed, c_0

Parameter values:
 $\lambda = 0.5, \Lambda = 0.7$
 For isothermal flow
 $c_0 = 3$

