

THERMALLY DRIVEN GRAVITY CURRENTS

PART 1: Formulation and Analytical Results

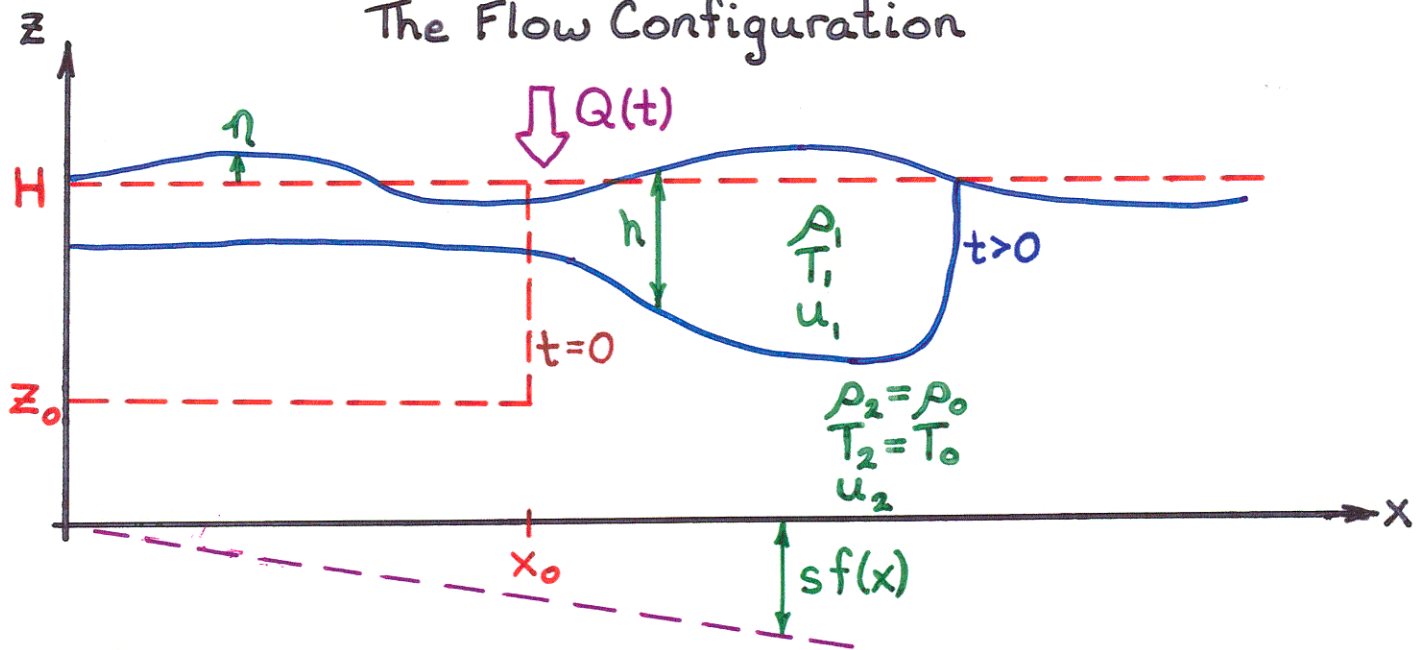
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The Flow Configuration



Model Assumptions and Approximations:

- inviscid fluid and incompressible & immiscible
- small aspect ratio, $\delta = H/L$, $0 < \delta \ll 1$
- pressure is hydrostatic to $O(\delta^2)$
- Boussinesq approximation
- temperature remains uniform throughout surface layer
- ignore heat transfer between the fluid layers
- equation of state given by:

$$\rho_1(T) = \rho_0 [1 - \alpha(T - T_0)^n], \quad n > 0$$

- ignore effects of surface tension

Planar Shallow Water Equations

In dimensionless form the governing equations become:

$$\begin{aligned}\frac{\partial u_1}{\partial t} + u_1 \frac{\partial u_1}{\partial x} + \left(1 - \frac{g'}{g} \theta^n\right) \frac{\partial \eta}{\partial x} &= 0 \\ \frac{\partial h}{\partial t} + \frac{\partial}{\partial x}(u_1 h) &= 0 \\ \frac{\partial u_2}{\partial t} + u_2 \frac{\partial u_2}{\partial x} + \frac{\partial \eta}{\partial x} - \theta^n \frac{\partial h}{\partial x} &= 0 \\ \frac{\partial}{\partial t} \left(h - \frac{g'}{g} \eta\right) + \frac{\partial}{\partial x} \left[u_2 \left(h - H - \frac{g'}{g} \eta - s f(x)\right)\right] &= 0 \\ \frac{d\theta}{dt} = Q(t), \quad \theta = \frac{T - T_0}{T_* - T_0}\end{aligned}$$

An important dimensionless parameter is given by:

$$\frac{g'}{g} = \frac{\rho_0 - \rho_*}{\rho_0} = \alpha(T_* - T_0)^n$$

where g' is the reduced gravity.

Initial and Boundary Conditions

The equations are posed as an initial value problem subject to:

$$u_1(x, 0) = 0, \quad u_2(x, 0) = 0, \quad \eta(x, 0) = 0, \quad \theta(0) = 1$$

$$h(x, 0) = \begin{cases} h_* & \text{for } x \leq x_0 \\ 0 & \text{for } x > x_0 \end{cases}$$

$$u_1(0, t) = 0, \quad u_2(0, t) = 0, \quad t > 0$$

$$\frac{\partial h}{\partial x}(0, t) = 0, \quad \frac{\partial \eta}{\partial x}(0, t) = 0, \quad t > 0$$

$$h \rightarrow 0, \quad \eta \rightarrow 0 \text{ as } x \rightarrow \infty$$

To close the system we need to specify $Q(t)$ & n .
We assume that $\theta(t)$ is known once $Q(t)$ is given.

We next identify two limiting cases:

- Weak Stratification Limit
- Deep Ambient Layer Limit

Weak Stratification Limit

If the initial density difference is small we can neglect terms of $O(g'/g)$. In this limit the governing equations can be simplified to (setting $H = 1$ and $s = 0$):

$$\frac{\partial u_1}{\partial t} + \left(\frac{1-3h}{1-h} \right) u_1 \frac{\partial u_1}{\partial x} + \left[\theta^n (1-h) - \frac{u_1^2}{(1-h)^2} \right] \frac{\partial h}{\partial x} = 0$$

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x}(u_1 h) = 0$$

$$\frac{d\theta}{dt} = Q(t)$$

$$\eta = -\frac{\theta^n}{2}(1-h)^2 - \frac{u_1^2 h}{1-h}, \quad u_2 = -\frac{u_1 h}{1-h}$$

Deep Ambient Layer Limit

If we let $H \rightarrow \infty$ with $h = O(1)$ and again ignore terms of $O(g'/g)$ and set $s = 0$ we obtain:

$$\frac{\partial u_1}{\partial t} + u_1 \frac{\partial u_1}{\partial x} + \theta^n \frac{\partial h}{\partial x} = 0$$

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x}(u_1 h) = 0$$

$$\frac{d\theta}{dt} = Q(t)$$

$$\frac{\partial \eta}{\partial x} = \theta^n \frac{\partial h}{\partial x}, \quad u_2 = 0$$

Analysis of Deep Ambient Layer System

Rewrite the equations in vector form:

$$\frac{\partial \mathbf{U}}{\partial t} + \frac{\partial}{\partial x} \mathbf{F}(\mathbf{U}, t) = 0$$

$$\frac{d\theta}{dt} = Q(t)$$

where

$$\mathbf{U} = \begin{pmatrix} u_1 \\ h \end{pmatrix}, \quad \mathbf{F} = \begin{pmatrix} \frac{1}{2}u_1^2 + \theta^n h \\ u_1 h \end{pmatrix}$$

The eigenvalues associated with the Jacobian matrix $\partial \mathbf{F} / \partial \mathbf{U}$ are:

$$\lambda^{\pm} = u_1 \pm \sqrt{\theta^n h}$$

Since λ^{\pm} are real, the system is hyperbolic and can be expressed in characteristic form as:

$$\frac{d}{dt} \{u_1 \pm 2\sqrt{\theta^n h}\} = \pm \frac{n\sqrt{\theta^n h}Q(t)}{\theta} \quad \text{along} \quad \frac{dx}{dt} = u_1 \pm \sqrt{\theta^n h}$$

Similarity Solutions

The deep ambient layer system admits similarity solutions for:

$$Q(t) = Q_0 \Rightarrow \theta(t) = 1 + Q_0 t \text{ and}$$

$$Q(t) = -k\theta \Rightarrow \theta(t) = e^{-kt}$$

For $Q(t) = Q_0$ we obtain:

$$u_1(x, t) = \left(t + \frac{1}{Q_0}\right)^{(n-1)/3} v(\xi), \quad h(x, t) = \left(t + \frac{1}{Q_0}\right)^{-(n+2)/3} f(\xi)$$

$$v(\xi) = \frac{(n+2)}{3}\xi, \quad f(\xi) = \frac{(n+2)}{18Q_0^n} [(2n+1)\xi_f^2 - (n-1)\xi^2]$$

$$\xi = x \left(t + \frac{1}{Q_0}\right)^{-(n+2)/3}, \quad \xi_f = 3 \left(\frac{2Q_0^n h_* x_0}{(n+2)(5n+4)}\right)^{1/3}$$

The shock front speed is given by: $\dot{x}_f = \xi_f \frac{(n+2)}{3} \left(t + \frac{1}{Q_0}\right)^{(n-1)/3}$

For $Q(t) = -k\theta$ we obtain:

$$u_1(x, t) = e^{-nkt/3} v(\xi), \quad h(x, t) = e^{nkt/3} f(\xi)$$

$$v(\xi) = -\frac{nk}{3}\xi, \quad f(\xi) = \frac{n^2 k^2}{18} [2\xi_f^2 - \xi^2]$$

$$\xi = x e^{nkt/3}, \quad \xi_f = 3 \left(\frac{2h_* x_0}{5n^2 k^2}\right)^{1/3}$$

The shock front speed is given by: $\dot{x}_f = -\xi_f \frac{nk}{3} e^{-nkt/3}$

Analysis of Weak Stratification System

Rewrite the equations in vector form:

$$\frac{\partial \mathbf{U}}{\partial t} + \frac{\partial}{\partial x} \mathbf{F}(\mathbf{U}, t) = 0$$

$$\frac{d\theta}{dt} = Q(t)$$

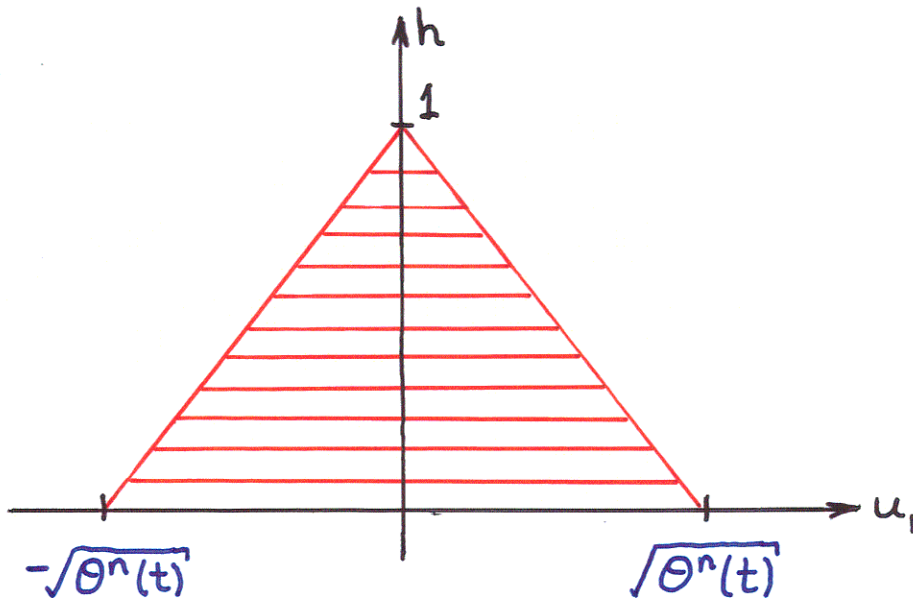
where

$$\mathbf{U} = \begin{pmatrix} u_1 \\ h \end{pmatrix}, \quad \mathbf{F} = \begin{pmatrix} \frac{1}{2}u_1^2 + \eta(u_1, h, \theta) \\ u_1 h \end{pmatrix}, \quad \eta = -\frac{\theta^n}{2}(1-h)^2 - \frac{u_1^2 h}{1-h}$$

The eigenvalues associated with the Jacobian matrix $\partial \mathbf{F} / \partial \mathbf{U}$ are:

$$\lambda^{\pm} = \frac{u_1(1-2h)}{1-h} \pm \frac{1}{1-h} \sqrt{h(1-h)[(1-h)^2 \theta^n - u_1^2]}$$

The region of hyperbolicity satisfies: $(1-h)^2 \theta^n - u_1^2 \geq 0$



The weakly stratified system can be cast in characteristic form:

$$\frac{du_1}{dt} + \left\{ \frac{u_1}{1-h} \pm \sqrt{\frac{1-h}{h}} \sqrt{\theta^n - \frac{u_1^2}{(1-h)^2}} \right\} \frac{dh}{dt} = 0$$

$$\text{along } \frac{dx}{dt} = \frac{u_1(1-2h)}{1-h} \pm \sqrt{h(1-h)} \sqrt{\theta^n - \frac{u_1^2}{(1-h)^2}}$$

which can be further simplified to:

$$\frac{d}{dt} \left\{ \arcsin \left(\frac{u_1}{(1-h)\sqrt{\theta^n}} \right) \pm \arcsin \left(2\left(h - \frac{1}{2}\right) \right) \right\} = -\frac{nu_1 Q(t)}{2\theta \sqrt{(1-h)^2 \theta^n - u_1^2}}$$

$$\text{along } \frac{dx}{dt} = \frac{u_1(1-2h)}{1-h} \pm \sqrt{h(1-h)} \sqrt{\theta^n - \frac{u_1^2}{(1-h)^2}}$$

The nonlinear nature of the characteristic fields is assessed using:

$$\text{grad}_{\mathbf{U}} \lambda^{\pm} \cdot \mathbf{v}^{\pm}$$

where \mathbf{v}^{\pm} are the eigenvectors of the Jacobian matrix.

The characteristic fields, $\lambda^{\pm}(\mathbf{U})$, are locally linearly degenerate about the state $u_1 = 0$, $h = 1/2$.

This may signal a bifurcation in the flow behaviour.

We explore this further using a weakly nonlinear analysis.

Weakly Nonlinear Analysis

We begin by expanding the variables about the basic state $(u_1, h) = (0, h_*)$ and work with the quadratically nonlinear system:

$$\frac{\partial \hat{u}}{\partial t} + \frac{(1 - 3h_*)}{(1 - h_*)} \hat{u} \frac{\partial \hat{u}}{\partial x} + \theta^n (1 - h_* - \hat{h}) \frac{\partial \hat{h}}{\partial x} = 0$$

$$\frac{\partial \hat{h}}{\partial t} + (h_* + \hat{h}) \frac{\partial \hat{u}}{\partial x} + \hat{u} \frac{\partial \hat{h}}{\partial x} = 0$$

These equations can be combined to yield the single equation:

$$\hat{h}_{tt} - h_*(1 - h_*)\theta^n \hat{h}_{xx} = -(\hat{u}\hat{h})_{xt} - h_*\theta^n(\hat{h}\hat{h}_x)_x + \frac{(1 - 3h_*)h_*}{(1 - h_*)}(\hat{u}\hat{u}_x)_x$$

We illustrate the procedure for the specific case $Q(t) = Q_0$ and $n = 2$ with $0 < Q_0 = \varepsilon \ll 1$. Thus, $\theta(t) = 1 + \varepsilon t$.

Next, we introduce the coordinates and series expansions given by:

$$\xi = x - c(t)t, \quad \eta = x + c(t)t, \quad T = \varepsilon t$$

where $c(t) = c_0(1 + \frac{\varepsilon}{2}t)$ and $c_0 = \sqrt{h_*(1 - h_*)}$

$$\hat{h} = \varepsilon h^{(0)}(\xi, \eta, T) + \varepsilon^2 h^{(1)}(\xi, \eta, T) + \dots$$

$$\hat{u} = \varepsilon u^{(0)}(\xi, \eta, T) + \varepsilon^2 u^{(1)}(\xi, \eta, T) + \dots$$

The $O(\varepsilon)$ Problem:

$$h_{\eta\xi}^{(0)} = 0$$

$$c_0(\partial_\eta - \partial_\xi)u^{(0)} = -(1 - h_*)(1 + T)(\partial_\eta + \partial_\xi)h^{(0)}$$

These can be easily solved to give:

$$h^{(0)} = \phi(\xi, T) + \psi(\eta, T)$$

$$u^{(0)} = \frac{(1 - h_*)(1 + T)}{c_0}(\phi(\xi, T) - \psi(\eta, T))$$

The $O(\varepsilon^2)$ Problem:

$$-4c_0^2 h_{\eta\xi}^{(1)} = A(\xi, T) + B(\xi, \eta, T) + C(\eta, T)$$

where

$$A(\xi, T) = \frac{2c_0}{(1 + T)}\phi_{T\xi} + \frac{3}{2}(1 - 2h_*)(\phi^2)_{\xi\xi}$$

$$B(\xi, \eta, T) = -(1 - 2h_*)[\phi\psi_{\eta\eta} + \psi\phi_{\xi\xi} + 2\psi_\eta\phi_\xi]$$

$$C(\eta, T) = -\frac{2c_0}{(1 + T)}\psi_{T\eta} + \frac{3}{2}(1 - 2h_*)(\psi^2)_{\eta\eta}$$

Imposing the solvability condition $A = 0$ and integrating yields:

$$\phi_T + \frac{3(1 - 2h_*)(1 + T)}{2c_0} \phi \phi_\xi = 0$$

If $\phi(\xi, 0) = f(\xi)$ then the solution can be expressed implicitly in terms of the parameter s as:

$$\phi(\xi, T) = f(s) \quad \text{along} \quad \xi = \frac{3(1 - 2h_*)}{4c_0} [(1 + T)^2 - 1] f(s) + s$$

Shock formation occurs when $|\phi_\xi| \rightarrow \infty$ where

$$\phi_\xi = \frac{4c_0 f'(s)}{4c_0 + 3(1 - 2h_*) f'(s) [(1 + T)^2 - 1]}$$

which becomes infinite when

$$T(s) = -1 \pm \sqrt{1 - K(s)}, \quad K(s) = \frac{4c_0}{3(1 - 2h_*) f'(s)}$$

Thus, a shock will form for $T > 0$ when $K(s) < 0$.

For $f'(s) > 0$ (corresponding to the back side of the rightward propagating smooth initial wave) this will happen provided

$$h_* > 1/2.$$

A similar conclusion follows from the solvability condition $C = 0$.