Long-wave instability of flow with temperature dependent fluid properties down an incline

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# **Problem Description**

We consider two-dimensional gravity-driven flow of a thin fluid layer having variable fluid properties down a heated incline as shown:



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# **Previous Work**

- Isothermal flow has been studied extensively experimentally (initially by Kapitza & Kapitza, 1949), theoretically (initially by Benjamin, 1957) and using DNS (initially by Ramaswamy, Chippada & Joo, 1996). Commonly used mathematical models include the integral-boundary-layer model (Shkadov, 1967) and the weighted residual model (Ruyer-Quil & Manneville, 2002).
- Non-isothermal flow has received much less attention. The focus has been on the variation of surface tension with temperature which gives rise to the Marangoni effect. A key contribution was by Trevelyan *et al.* (2007). The studies by Goussis & Kelly (1985) and Hwang & Weng (1988) considered variations in viscosity only, while Kabova & Kuznetsov (2002) accounted for variable viscosity and surface tension.

In the current study we investigate the influence that variable surface tension ( $\sigma$ ), density ( $\rho$ ), viscosity ( $\mu$ ), thermal conductivity (K) and specific heat ( $c_{\rho}$ ) have on the stability of the flow.

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# Mathematical Formulation

For flow with variable fluid properties the governing equations in the absence of viscous dissipation are (Spurk & Aksel, 2008):

$$\begin{aligned} \frac{D\rho}{Dt} + \rho \left( \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) &= 0 \\ \rho \frac{Du}{Dt} &= -\frac{\partial p}{\partial x} + g\rho \sin\beta + \frac{\partial}{\partial x} \left[ 2\mu \frac{\partial u}{\partial x} - \frac{2}{3}\mu \left( \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) \right] \\ &+ \frac{\partial}{\partial z} \left[ \mu \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \right] \\ \rho \frac{Dw}{Dt} &= -\frac{\partial p}{\partial z} - g\rho \cos\beta + \frac{\partial}{\partial z} \left[ 2\mu \frac{\partial w}{\partial z} - \frac{2}{3}\mu \left( \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) \right] \\ &+ \frac{\partial}{\partial x} \left[ \mu \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \right] \\ \rho \frac{D(c_{\rho}T)}{Dt} &= \frac{\partial}{\partial x} \left( K \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial z} \left( K \frac{\partial T}{\partial z} \right) - p \left( \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) \end{aligned}$$

 $(\partial x \ \partial z)$ 

# Variable Fluid Properties

The fluid properties are assumed to vary linearly with temperature as follows:

$$\rho = \rho_0 - \hat{\alpha}(T - T_a)$$
$$\mu = \mu_0 - \hat{\lambda}(T - T_a)$$
$$c_p = c_{p0} + \hat{S}(T - T_a)$$
$$K = K_0 + \hat{\Lambda}(T - T_a)$$
$$\sigma = \sigma_0 - \gamma(T - T_a)$$

where  $\rho_0$ ,  $\mu_0$ ,  $c_{\rho 0}$ ,  $K_0$  and  $\sigma_0$  are reference values at  $T = T_a$ .



# **Dimensionless Equations**

Using the Boussinesq approximation and the proposed scaling we obtain:

$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

$$Re\frac{Du}{Dt} = -Re\frac{\partial p}{\partial x} + 3(1 - \alpha T) + \frac{\partial}{\partial x} \left( (1 - \lambda T) \frac{\partial u}{\partial x} \right) + \frac{\partial}{\partial z} \left( (1 - \lambda T) \frac{\partial u}{\partial z} \right)$$

$$-\lambda \frac{\partial T}{\partial x} \frac{\partial u}{\partial x} - \lambda \frac{\partial T}{\partial z} \frac{\partial w}{\partial x}$$

$$Re\frac{Dw}{Dt} = -Re\frac{\partial p}{\partial z} - 3\cot\beta(1 - \alpha T) + \frac{\partial}{\partial x} \left( (1 - \lambda T) \frac{\partial w}{\partial x} \right) + \frac{\partial}{\partial z} \left( (1 - \lambda T) \frac{\partial w}{\partial z} \right)$$

$$-\lambda \frac{\partial T}{\partial x} \frac{\partial u}{\partial z} - \lambda \frac{\partial T}{\partial z} \frac{\partial w}{\partial z}$$

$$PrRe\frac{D}{Dt} \left[ \left( 1 + \frac{S}{\Delta T_r} \right) T + ST^2 \right] = \frac{\partial}{\partial x} \left[ (1 + \Lambda T) \frac{\partial T}{\partial x} \right] + \frac{\partial}{\partial z} \left[ (1 + \Lambda T) \frac{\partial T}{\partial z} \right]$$

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# **Boundary Conditions**

Along the free surface z = h:

$$p = \frac{2(1 - \lambda T)}{ReF} \left( \left[ \frac{\partial h}{\partial x} \right]^2 \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} - \frac{\partial h}{\partial x} \frac{\partial u}{\partial z} - \frac{\partial h}{\partial x} \frac{\partial w}{\partial x} \right) - \frac{(We - MaT)}{F^{3/2}} \frac{\partial^2 h}{\partial x^2}$$
$$-MaRe\sqrt{F} \left( \frac{\partial T}{\partial x} + \frac{\partial h}{\partial x} \frac{\partial T}{\partial z} \right) = (1 - \lambda T) \left[ G \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) - 4 \frac{\partial h}{\partial x} \frac{\partial u}{\partial x} \right]$$
$$w = \frac{\partial h}{\partial t} + u \frac{\partial h}{\partial x}$$
$$-Bi\sqrt{F}T = (1 + \Lambda T) \left( \frac{\partial T}{\partial z} - \frac{\partial h}{\partial x} \frac{\partial T}{\partial x} \right)$$
where  $F = 1 + \left[ \frac{\partial h}{\partial x} \right]^2$ ,  $G = 1 - \left[ \frac{\partial h}{\partial x} \right]^2$ 

On the bottom z = 0: u = w = 0, T = 1

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# **Dimensionless Parameters**



Also,  $\alpha$ ,  $\lambda$ ,  $\Lambda$ , S represent dimensionless rates of change of density, viscosity, thermal conductivity and specific heat with respect to temperature.

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# **Steady State Equations**

Steady uniform flow in the streamwise direction given by  $h \equiv 1$ ,  $w \equiv 0$ ,  $u = u_s(z)$ ,  $p = p_s(z)$  and  $T = T_s(z)$  satisfies the following boundary-value problems:

$$\frac{d}{dz} \left[ (1 + \Lambda T_s) \frac{dT_s}{dz} \right] = 0 , \ (1 + \Lambda T_s) \frac{dT_s}{dz} + BiT_s = 0 \text{ at } z = 1 , \ T_s(0) = 1$$
$$\frac{d}{dz} \left[ (1 - \lambda T_s) \frac{du_s}{dz} \right] + 3(1 - \alpha T_s) = 0 , \ \frac{du_s}{dz} = 0 \text{ at } z = 1 , \ u_s(0) = 0$$
$$Re \frac{dp_s}{dz} = -3 \cot\beta(1 - \alpha T_s) , \ p_s(1) = 0$$



# **Steady State Solutions**

The steady state solutions are given by:

$$T_s(z) = \sqrt{a - bz} - \frac{1}{\Lambda}$$

$$u_{s}(z) = a_{0} \ln \left(\frac{A - \lambda\sqrt{a - bz}}{A - \lambda\sqrt{a}}\right) + a_{1}z - \frac{\alpha}{\lambda}z^{2} + a_{2}(\sqrt{a - bz} - \sqrt{a})$$
$$+a_{3}[(a - bz)^{3/2} - a^{3/2}]$$
$$p_{s}(z) = \frac{3\cot\beta}{Re} \left(1 + \frac{\alpha}{\Lambda}\right)(1 - z) + \frac{2\alpha\cot\beta}{bRe}[(a - b)^{3/2} - (a - bz)^{3/2}]$$
where the constants *a*, *b*, *a*<sub>0</sub>, *a*<sub>1</sub>, *a*<sub>2</sub>, *a*<sub>3</sub> and *A* are related to the

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parameters  $\Lambda$ , Bi,  $\lambda$  and  $\alpha$ .

# **Stability Analysis**

Now impose small disturbances on the steady state flow:

$$u = u_s(z) + \tilde{u}(x, z, t) , w = \tilde{w}(x, z, t) , p = p_s(z) + \tilde{p}(x, z, t)$$
$$T = T_s(z) + \tilde{T}(x, z, t) , h = 1 + \eta(x, t)$$

Next, substitute these into the governing equations, linearize and assume the disturbances have the form:

$$(\tilde{u}, \tilde{w}, \tilde{p}, \tilde{T}, \eta) = (\hat{u}(z), \hat{w}(z), \hat{p}(z), \hat{T}(z), \hat{\eta})e^{ik(x-ct)}$$

where k (real & positive) represents the wavenumber of the perturbation and c is a complex quantity with the real part denoting the phase speed of the perturbation while the imaginary part is related to the growth rate.



# **Perturbation Equations**

The linearized perturbed equations become:

$$D\hat{w} + ik\hat{u} = 0$$

$$\begin{aligned} ℜ[ik(u_s - c)\hat{u} + \hat{w}Du_s] = -ikRe\hat{p} + k^2(\lambda T_s - 1)\hat{u} \\ &+ D[(1 - \lambda T_s)D\hat{u}] - \lambda \hat{T}D^2u_s - \lambda Du_sD\hat{T} - ik\lambda\hat{w}DT_s - 3\alpha\hat{T} \\ &ikRe(u_s - c)\hat{w} = -ReD\hat{p} + 3\alpha\cot\beta\hat{T} - k^2(1 - \lambda T_s)\hat{w} \\ &+ D[(1 - \lambda T_s)D\hat{w}] - ik\lambda\hat{T}Du_s - \lambda DT_sD\hat{w} \\ &PrRe(1 + S/\Delta T_r + 2ST_s)[ik(u_s - c)\hat{T} + \hat{w}DT_s] \\ &= -k^2(1 + \Lambda T_s)\hat{T} + D^2[(1 + \Lambda T_s)\hat{T}] \end{aligned}$$

where the differential operator *D* is defined as:

$$D \equiv rac{d}{dz}$$

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# **Boundary Conditions**

Along the free surface (z = 1) the perturbations will satisfy:

$$\hat{p} = -\hat{\eta}Dp_s + \frac{2}{Re}(1 - \lambda T_s)D\hat{w} + k^2(We - MaT_s)\hat{\eta}$$

$$(1 - \lambda T_s)(\hat{\eta}D^2u_s + D\hat{u} + ik\hat{w}) = -ikMaRe(\hat{T} + \hat{\eta}DT_s)$$

$$D[(1 + \Lambda T_s)\hat{T}] + \hat{\eta}D[(1 + \Lambda T_s)DT_s + BiT_s] + Bi\hat{T} = 0$$

$$\hat{w} = ik(u_s - c)\hat{\eta}$$

while the bottom conditions are:

$$\hat{u}(0) = \hat{w}(0) = \hat{T}(0) = 0$$



# Small Wavenumber Expansion

Since small wavenumber perturbations are expected to be the most unstable, we expand the perturbations in the following series:

$$\hat{u} = u_0(z) + ku_1(z) + O(k^2)$$
$$\hat{w} = w_0(z) + kw_1(z) + O(k^2)$$
$$\hat{p} = p_0(z) + kp_1(z) + O(k^2)$$
$$\hat{T} = T_0(z) + kT_1(z) + O(k^2)$$
$$\hat{\eta} = \eta_0 + k\eta_1 + O(k^2)$$
$$c = c_0 + kc_1 + O(k^2)$$

and proceed to solve the eigenvalue problem asymptotically as  $k \rightarrow 0$ .

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# **Special Cases:**

For Bi = 0 the critical Reynolds number for the onset of instability can be found exactly and is given by:

$${\it Re}_{\it crit} = rac{5}{6} \cot eta rac{(1-\lambda)^2}{(1-lpha)}$$

Note that if the values of  $\alpha$  and  $\lambda$  are such that  $1 - \alpha = (1 - \lambda)^2$ , then it follows that the effects of variable fluid properties cancel and the threshold of instability is the same as that for isothermal flow. Other special cases include  $\Lambda = \lambda = 0$  and  $Bi \rightarrow \infty$ , both of which lead to exact, but lengthy, expressions for  $Re_{crit}$ . For the general case, analytical expressions for the neutral stability state have been obtained in the form of asymptotic expansions as  $Bi \rightarrow 0$  or as  $\Lambda$ ,  $\lambda \rightarrow 0$ .

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Accuracy of the expansion as  $Bi \rightarrow 0$ 

Parameters:  $\lambda = \Lambda = 0$  $\alpha = 0.6$ , S = 0,  $\Delta T_r = 1$ Ma = 1 and Pr = 7

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Accuracy of the expansion as  $\lambda \rightarrow 0$ 



### Steady-state temperature as a function of z



#### Parameters: $\Lambda = 0.5$



### Steady-state velocity as a function of z



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### Scaled critical Reynolds number as a function of $\boldsymbol{\lambda}$

Parameters: Bi = 0.25 $\alpha = 0.5$ , S = 1, Ma = 1 $\Delta T_r = 1$  and Pr = 7



### Scaled critical Reynolds number as a function of $\lambda$



Parameters: Bi = 0.25 $\alpha = 0.5$ , S = 1, Ma = 1 $\Lambda = 1$  and Pr = 7





### Scaled critical Reynolds number as a function of $\boldsymbol{\alpha}$

Parameters: Bi = 0.25 $\lambda = 0.2, \Lambda = 1, Ma = 1$  $\Delta T_r = 1$  and Pr = 7





### Scaled critical Reynolds number as a function of $\alpha$

Parameters: Bi = 0.25 $\lambda = 0, S = 1, \Lambda = 0.5$  $\Delta T_r = 1$  and Pr = 7





### Scaled critical Reynolds number as a function of Ma

 $\alpha = 0.5, S = 1, \Lambda = 0.5$  $\Delta T_r = 1$  and Pr = 7





### Scaled critical Reynolds number as a function of Bi

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# Conclusions

Through a combination of special cases and asymptotic expansions focussing on long-wave perturbations, our linear stability analysis uncovered the following key results:

If Bi = 0, then the critical Reynolds number for the onset of instability is given by:

$${\it Re}_{\it crit} = rac{5}{6} \cot eta rac{(1-\lambda)^2}{(1-lpha)}$$

- If Λ = λ = 0 an exact lengthy expression for *Re<sub>crit</sub>* was obtained which reproduces known results when appropriate limits are taken.
- If Bi → ∞ another lengthy expression for Re<sub>crit</sub> was obtained which can confirm the result in the limit of large Bi.

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- Increasing \u03c6 decreases viscosity which destabilizes the flow.
- Increasing α decreases density which, in general, stabilizes the flow. Exceptions to this occur in extreme cases of large variations in the specific heat and for large Marangoni numbers.
- ▶ In general, increasing *Ma* destabilizes the flow.
- ► The behaviour of *Re<sub>crit</sub>* with *Bi* is more complicated. As *Bi* increases from zero *Re<sub>crit</sub>* initially decreases and reaches a minimum value; as *Bi* is increases further *Re<sub>crit</sub>* increases. The limiting values of *Re<sub>crit</sub>* as *Bi* → 0 and *Bi* → ∞ can be found.
- This research has recently appeared in the: International Journal of Engineering Science, 70, 73-90, 2013

